

Cone Angle Choices For Atmospheric Entry Vehicles: A Review

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IPPW-6
Atlanta, Georgia
June 23-27, 2008

Why Do Cone Angles Of Entry Probes And Landers Vary from 45° To 70° ?

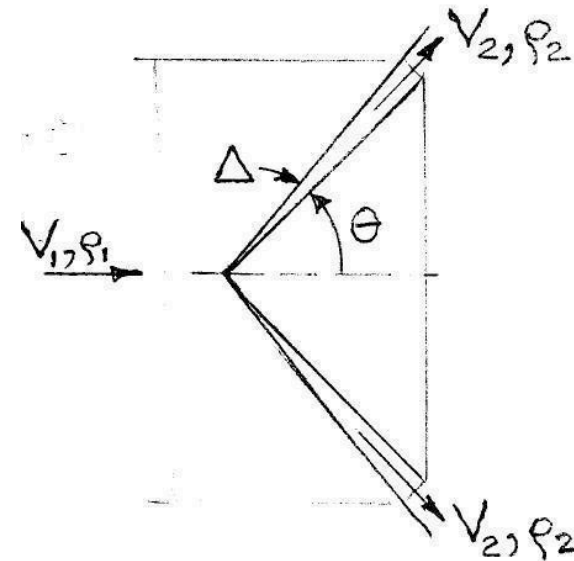
- Parameters that affect cone angle choices - packaging, atmosphere, heating, stability, etc.
 - Advantages of 45° cone angle
 - Packing of pressure vessels
 - Can decrease heating rates
 - High-speed dynamic stability
 - Larger cone angles
 - Decrease entry heating duration
 - Can increase heating rate, especially radiation
 - Increase descent heat conduction
 - Can decrease dynamic stability

- The thin conical shock layer, $\Delta \ll \Theta$, sharp nose, $\alpha = 0$, $\varepsilon = \rho_1 / \rho_2 \ll 1$

$$\frac{V_2}{V_1} = (1 - \Delta \tan \theta) \cos \theta$$

$$2\Delta^2 \tan \theta - (2 - \varepsilon)\Delta + \varepsilon \tan \theta = 0$$

$$\theta_{\max} = \tan^{-1} \left(\frac{2 - \varepsilon}{2\sqrt{2\varepsilon}} \right)$$



- Aerodynamic stability, $\alpha \ll \Theta$

$$C_L = 2(\cos^2 \theta - \sin^2 \theta)\alpha$$

$$\rightarrow \text{at } \theta = 45^\circ, \frac{dC_L}{d\alpha} = 0$$

- Entry trajectory and heating

Boundary layer; lam $n=0.5$, turb $n=0.8$

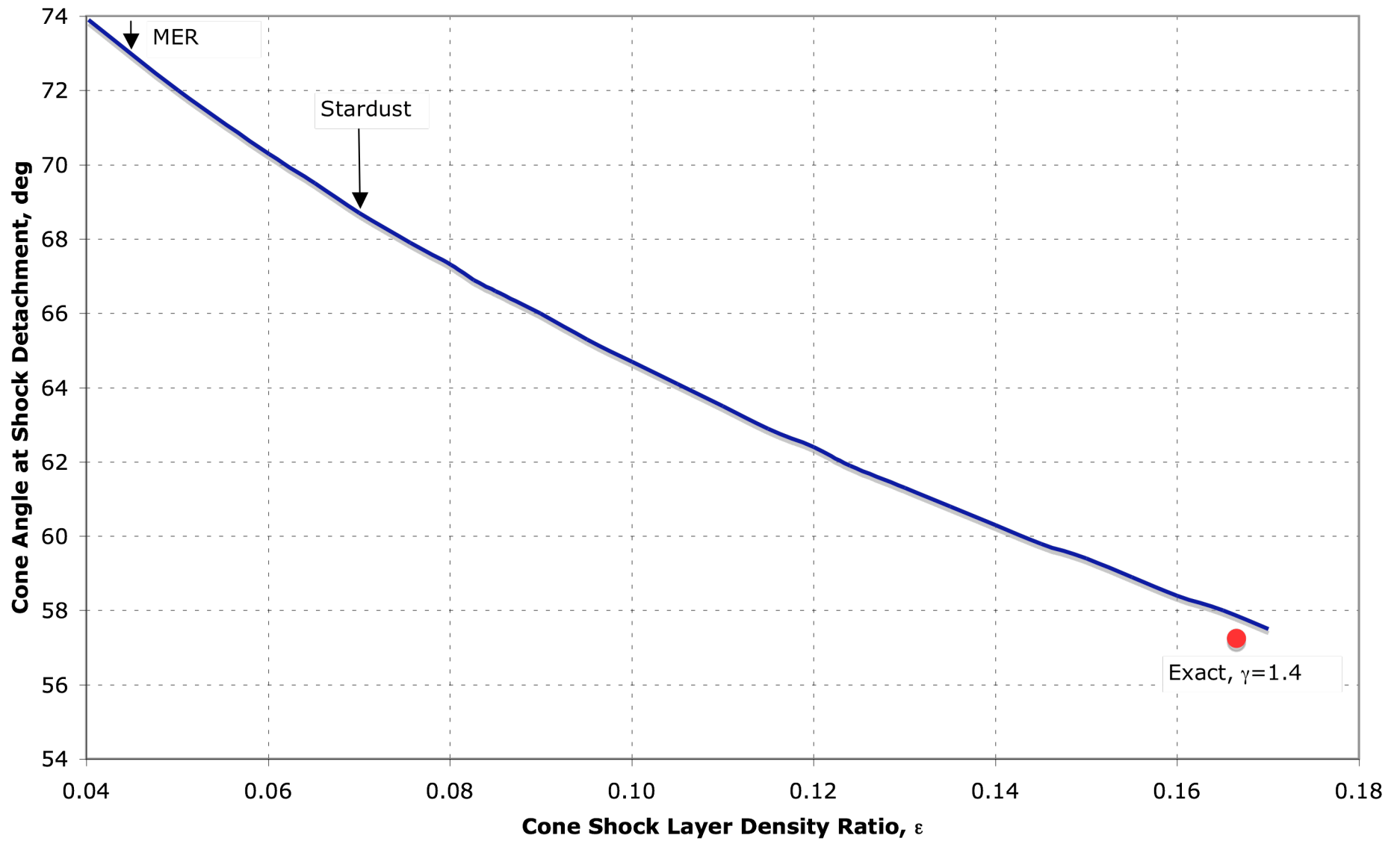
Radiation; inner planets $n=1.19-1.22$

Radiation; outer planets $n=1.17-1.45$

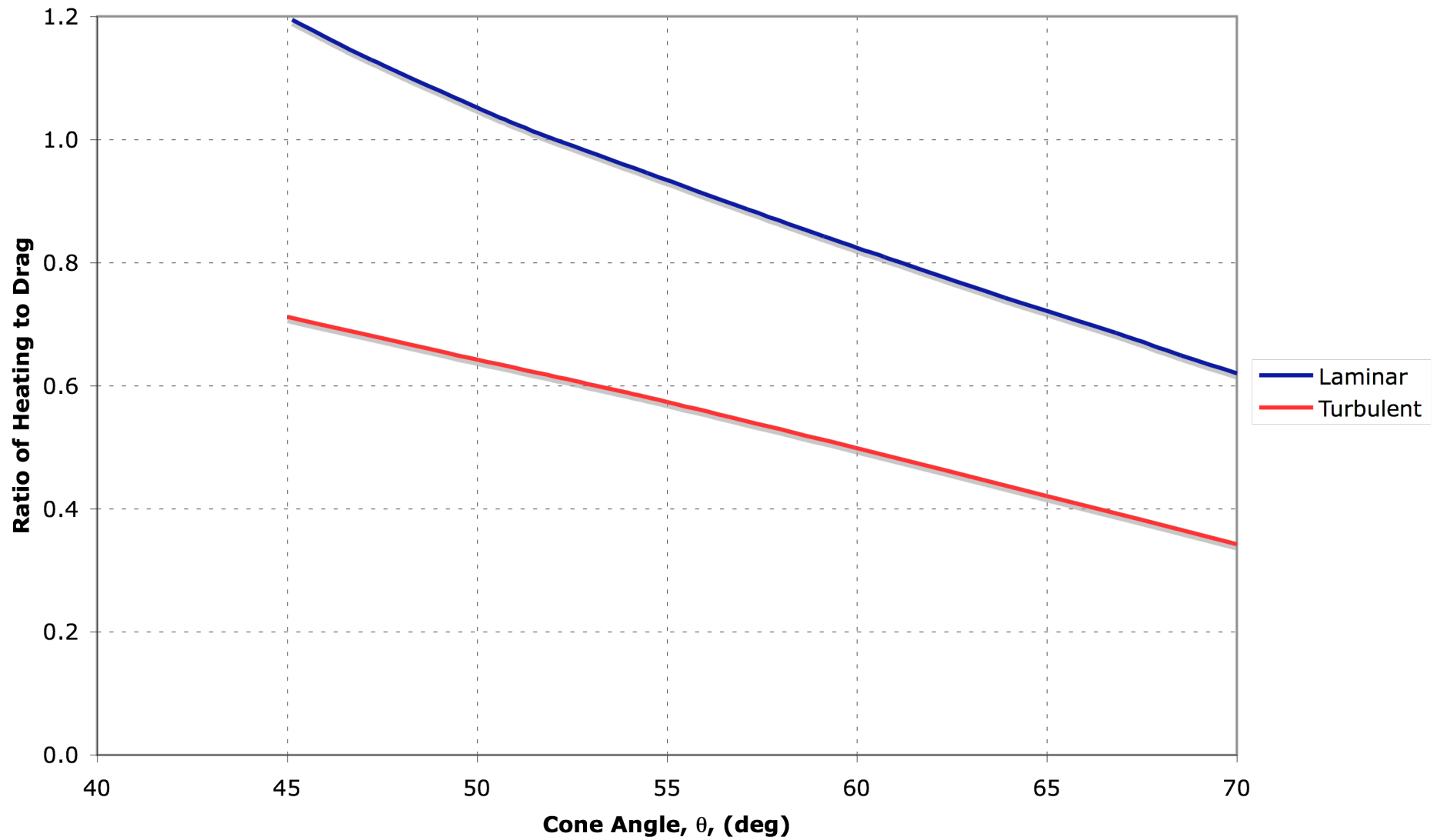
$$-\frac{dV}{dt} = \frac{D}{m} = \frac{1}{2\rho_1 V_1^2} \left(\frac{C_D A}{m} \right) \text{ and } \frac{dq}{dt} \sim \rho_1^n V_1^m$$

$$\rightarrow \text{heat load } q \sim \left(\frac{m}{C_D A} \right)^n$$

Conical Shock Detachment Conditions

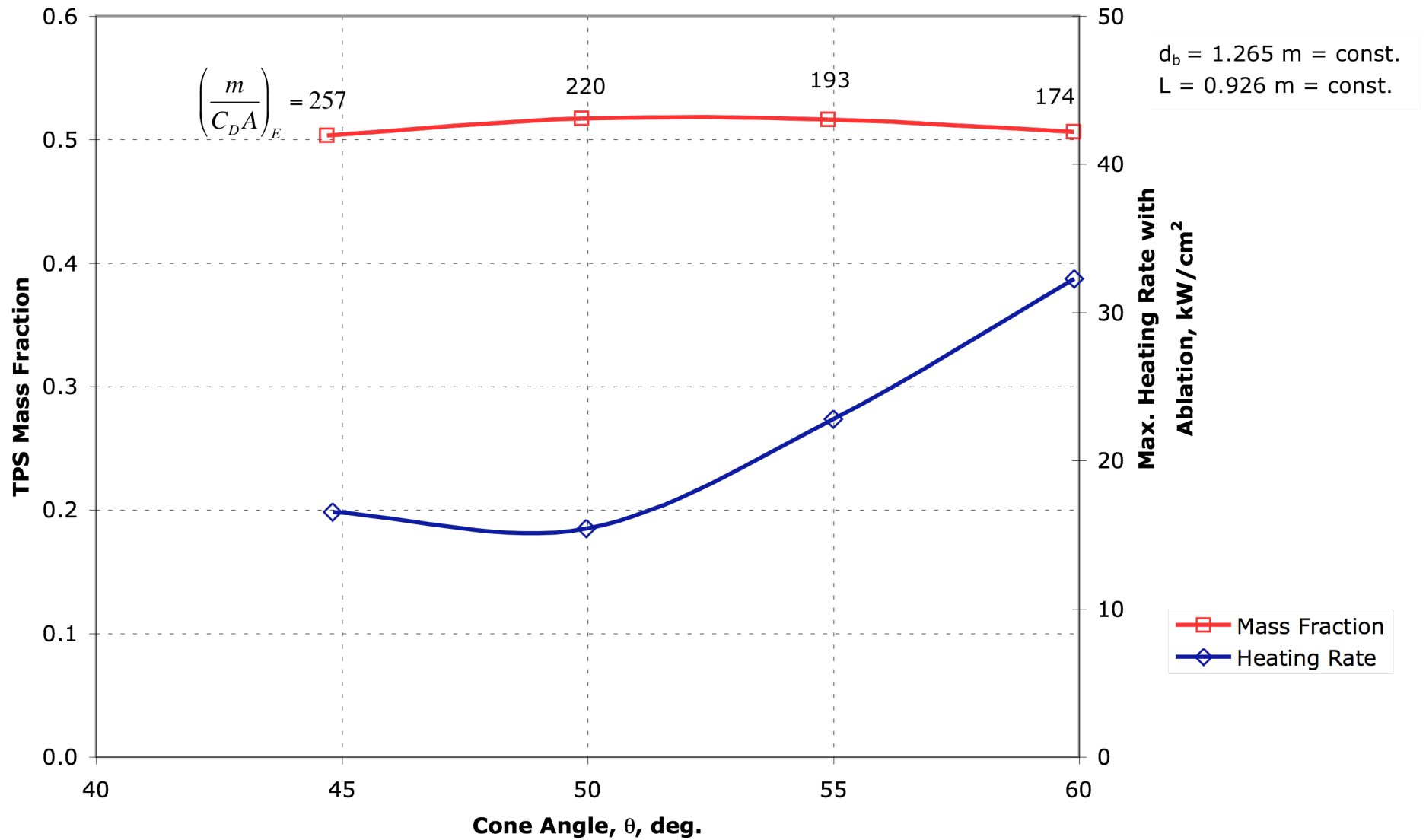


Convective Local Heat Load On Cone Frustum (Relative Values)

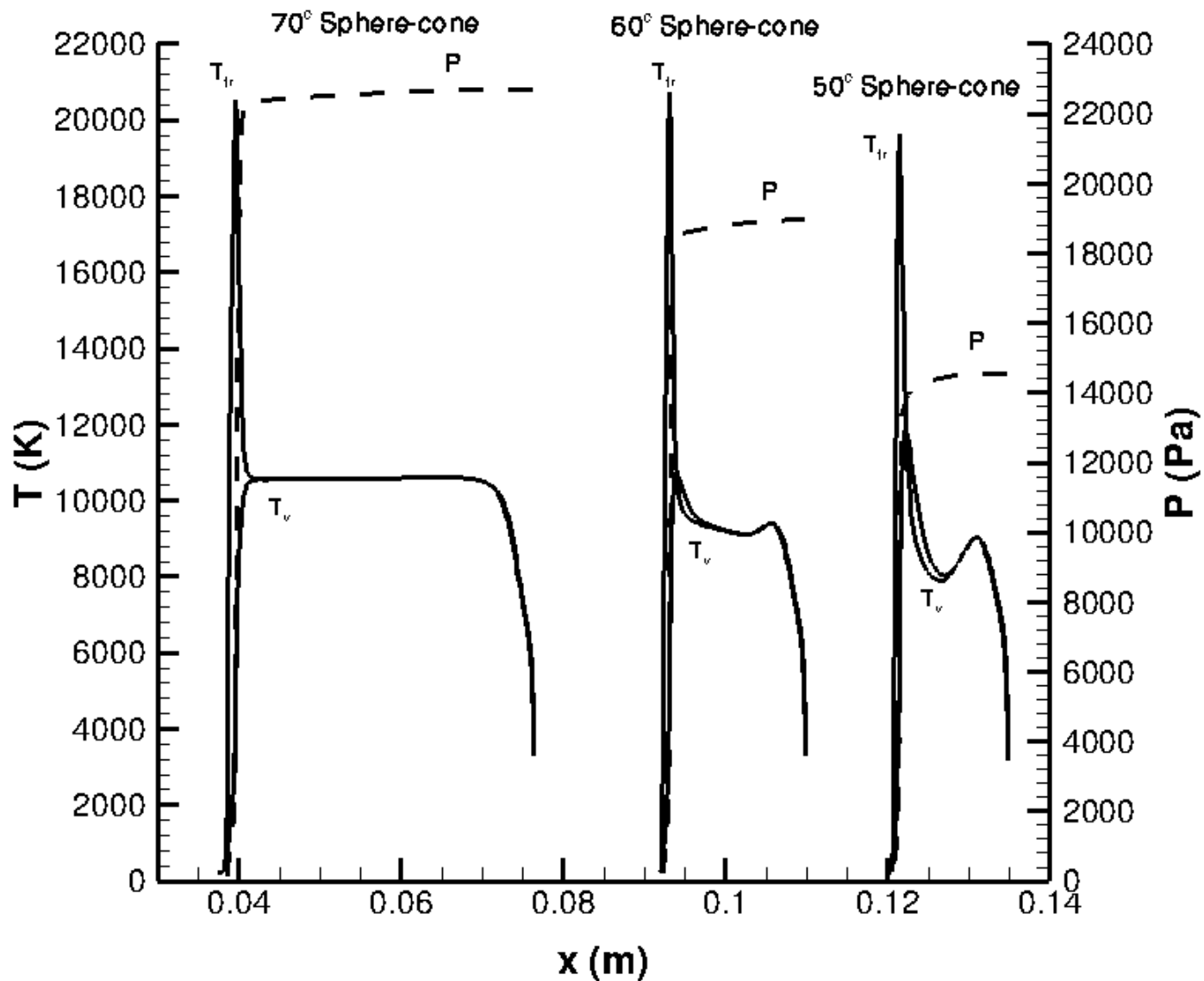


Variations Of Galileo Jupiter Probe

$m_E = 335 \text{ kg} = \text{const.}$

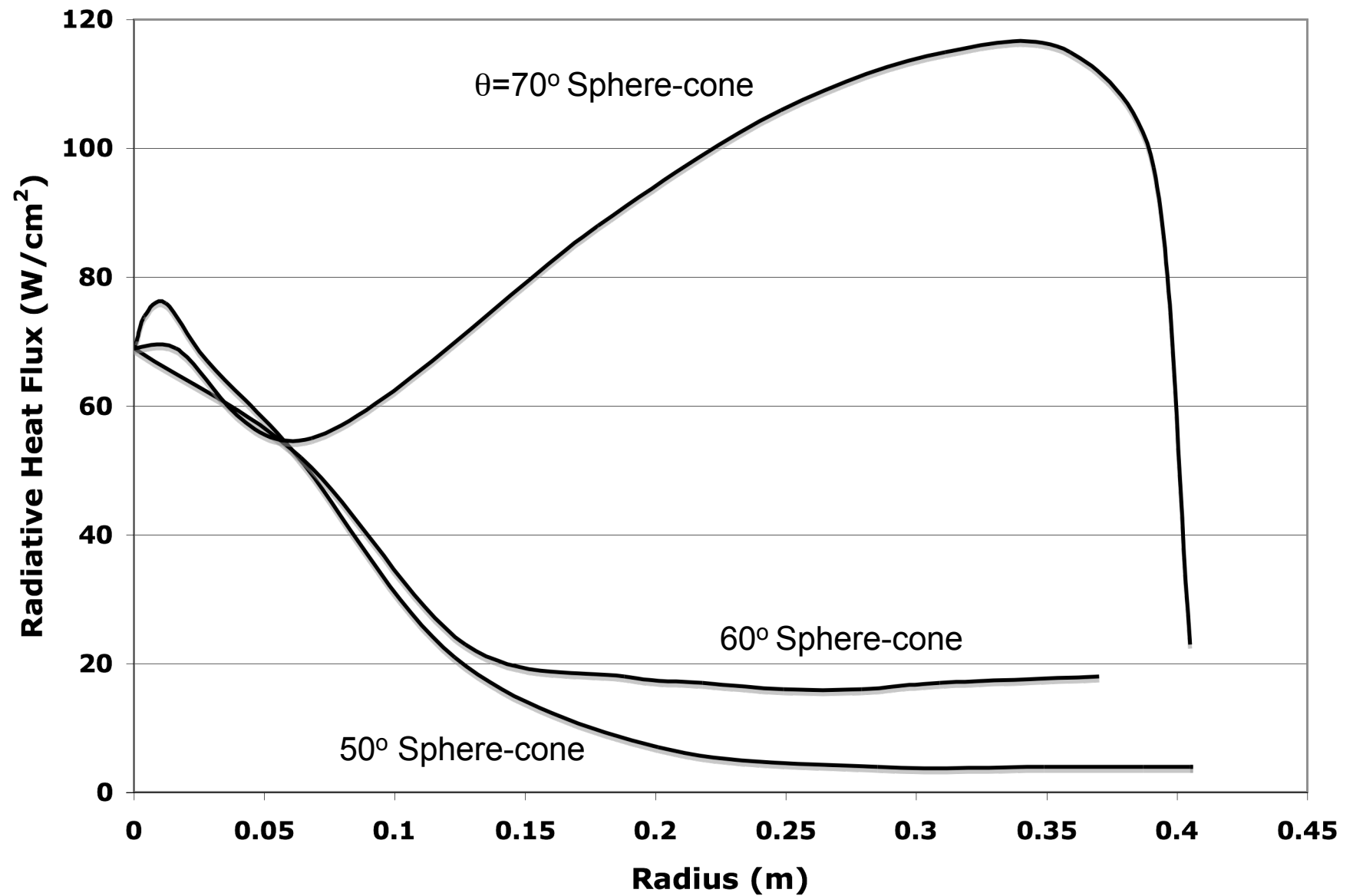


Shock Layer Temperature and Pressure Distributions at Cone Frustum Midpoints



$V = 10.871$ km/s, altitude = 61.761 km

Variations of Stardust Capsule



Heat Conduction During Descent

- Simplifying assumptions: terminal descent, exponential atm. density variation with altitude

$$mg \sin \gamma = D = \frac{1}{2} \rho V^2 C_D A$$

Since $\sin \gamma \rightarrow 1$ and $\rho \sim e^{-y/\eta}$, where η is atm. density scale height

$$dt = \frac{\eta}{\rho V} d\rho$$

Now the approximate descent time, t_d , becomes

$$t_d \sim \left(\frac{m}{C_D A} \right)^{-1/2} \left(\frac{\rho_o}{g} \right)^{1/2} \eta$$

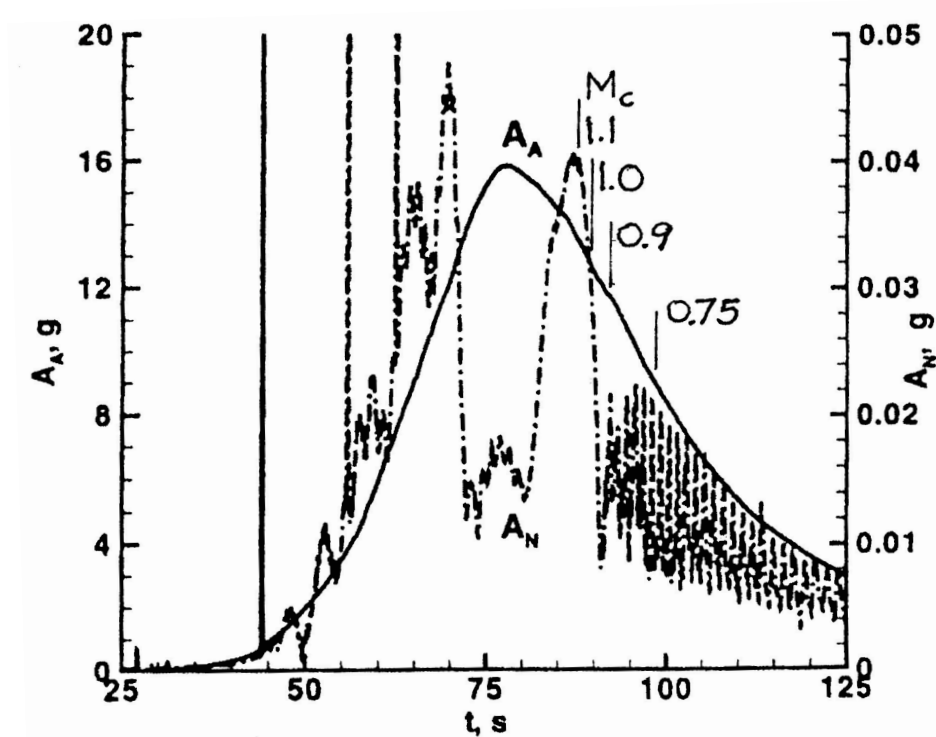
Where ρ_o is the atm. density where heat shield is discarded

- Note that heat conduction time is reduced by decreasing the C_D , or cone angle. In contrast, during entry the heat load is decreased by increasing the C_D , or cone angle

$$q \sim \left(\frac{m}{C_D A} \right)^n \text{ where } n > 0$$

- Also, note the effect of atm. density, ρ_o , and scale height, η , on the descent time

Mars Pathfinder Entry Dynamics

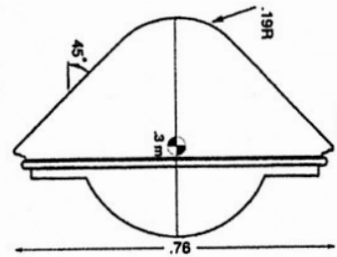


Total off-axis acceleration recorded during 100-s interval surrounding peak dynamic pressure.

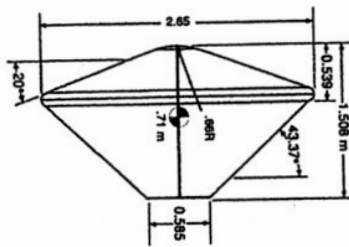
$$M_C = \frac{(\cot \theta)(1 - \frac{\epsilon \tan^2 \theta}{2 - \epsilon})}{\sqrt{\gamma \epsilon}}$$

Gnoffo, et al, "Prediction and Validation of Mars Pathfinder Hypersonic Aerodynamics Database," *Journal of Spacecraft and Rockets*, Vol. 36, No. 3, May-June 1999, pp. 367-373

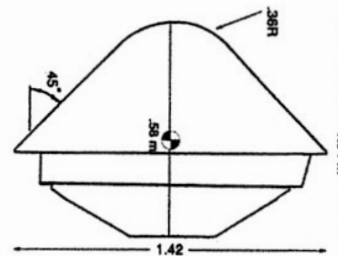
PLANETARY ATMOSPHERE ENTRY PROBE CONFIGURATIONS



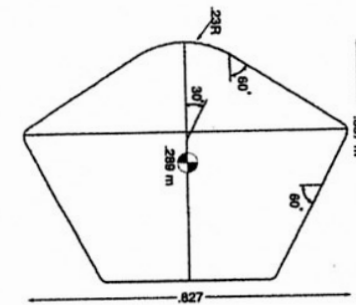
PIONEER VENUS
Small probe



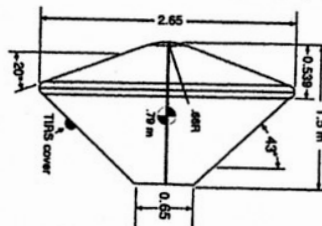
MARS PATHFINDER



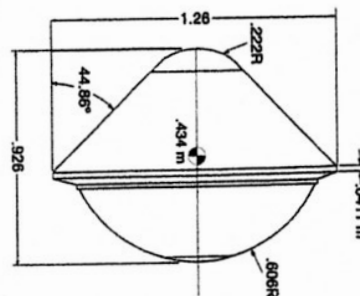
PIONEER VENUS
Large probe



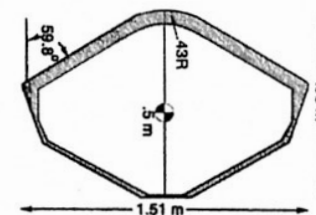
STARDUST
Earth



MARS EXPLORATION ROVER



GALILEO
Jupiter



GENESIS
Earth

Conclusions

Cone Angle	Planet(s)	V_E km/s	Atm.	Press. Vessel	Max. Heating w/o Ablat. kW/cm ²	Rel. Time	C_D
70°	Mars	6-7	Thin triatom.	no	Low (~0.1)	short	1.7
60°	Earth	11-13	Med. Diatom.	no	Med (~1.0)	Med.	1.5
45°	Venus	11-12	Dense triatom.	yes	High (~5.0)	Very long	1.0
45°	Jupiter	48	Med. Diatom.	yes	Severe (~50.0)	long	1.0
45°	Other outer planets	25-30	Med. Diatom.	yes	High (~5.0)	Very long - long	1.0

Back-up Slides

Variations Of Galileo Jupiter Probe

$$\left(\frac{m}{C_D A}\right)_E = 257 \text{ kg/m}^2 = \text{const.}$$

